

RESEARCH ARTICLES

Optimal requirements of a data acquisition system for a quadrupolar probe used in resistivity and permittivity surveys

Alessandro Settini^{1,*}, Achille Zirizzotti¹, James A. Baskaradas¹, Cesidio Bianchi¹

¹ Istituto Nazionale di Geofisica e Vulcanologia, Sezione Roma 2, Roma, Italy

Article history

Received May 27, 2010; accepted July 23, 2010.

Subject classification:

Instrumentation and techniques of general interest, Magnetic and electrical methods, Mathematical geophysics, Data processing.

ABSTRACT

This report discusses the development and engineering of a suitable quadrupolar probe for simultaneous and noninvasive surveys of electrical resistivity and dielectric permittivity. The quadrupolar probe can perform measurements on a subsurface with inaccuracies below a fixed limit (10%) in a bandwidth of low frequency (100 kHz). The quadrupole should be connected to an appropriate analog–digital converter that samples in phase and quadrature (IQ) or in uniform mode. If the probe is characterized by a galvanic contact with the surface, the inaccuracies in the measurements of resistivity and permittivity due to the IQ or uniform sampling analog–digital converter are analytically expressed. A large number of numerical simulations show that the performances of the probe depend on the selected sampler, and that the IQ is better compared to the uniform mode under the same operating conditions, i.e. for bit resolution and medium.

1. Introduction

Analog–digital converter

Typically, an analog–digital converter (ADC) [Razavi 1995] is an electronic device that converts an input analog voltage (or current) into a digital number. A sampler has several sources of errors. The accuracy is mainly limited by quantitation error. However, accurate reproduction is only possible if the sampling rate is more than twice the highest frequency of the signal. This is essentially what is embodied in the Shannon-Nyquist sampling theorem.

Different users of sampler models are interested in different modeling details, and so numerous models have been proposed in the literature. Some of these describe specific error sources [Polge et al. 1975], others are devised to connect conversion techniques and the corresponding errors [Arpaia et al. 1999, Arpaia et al. 2004].

Resistivity and permittivity surveys

Electrical resistivity and dielectric permittivity are two independent physical properties that characterize the behavior of bodies excited by an electromagnetic field. The

measurements of these properties provides crucial information regarding the practical uses of bodies (for example, materials that conduct electricity), and for countless other purposes.

Some studies have shown that the electrical resistivity and dielectric permittivity of a body can be obtained by measuring the complex impedance using a system with four electrodes, although these electrodes do not require resistive contact with the investigated body [Grard 1990a, Grard 1990b, Grard and Tabbagh 1991, Tabbagh et al. 1993, Vannaroni et al. 2004, Del Vento and Vannaroni 2005]. In this case, the current is made to circulate in the body by electric coupling, supplying the electrodes with an alternating electrical signal of low (LF) or middle (MF) frequency. In this type of investigation, the range of the optimal frequencies for electrical resistivity values of the more common materials is between ≈ 10 kHz and ≈ 1 MHz. Once complex impedance has been acquired, the distributions of the resistivity and permittivity in the investigated body can be estimated using well-known algorithms of inversion techniques.

Applying the same principle, but limited to the acquisition of resistivity only, there are various commercial instruments that are used in geology for investigating the first 2-5 m beneath the ground, both for the exploration of environmental areas and for archeological investigations [Samouëlian et al. 2005].

For the direct determination of the dielectric permittivity in the subsoil, besides geo-radar that can provide an estimate by complex measurement procedures on radar-gram processing [Declerk 1995, Sbartaï et al. 2006], the only technical instrument currently in use is known as the time-domain reflectometer. Time-domain reflectometers use two electrodes that are inserted deep into the ground, to acquire the dielectric permittivity in the subsoil for further analysis [Mojid et al. 2003, Mojid and Cho 2004].

Topic and structure of the report

This report presents a discussion of theoretical modeling, and moves towards the practical implementation of a quadrupolar probe that acquires complex impedance in

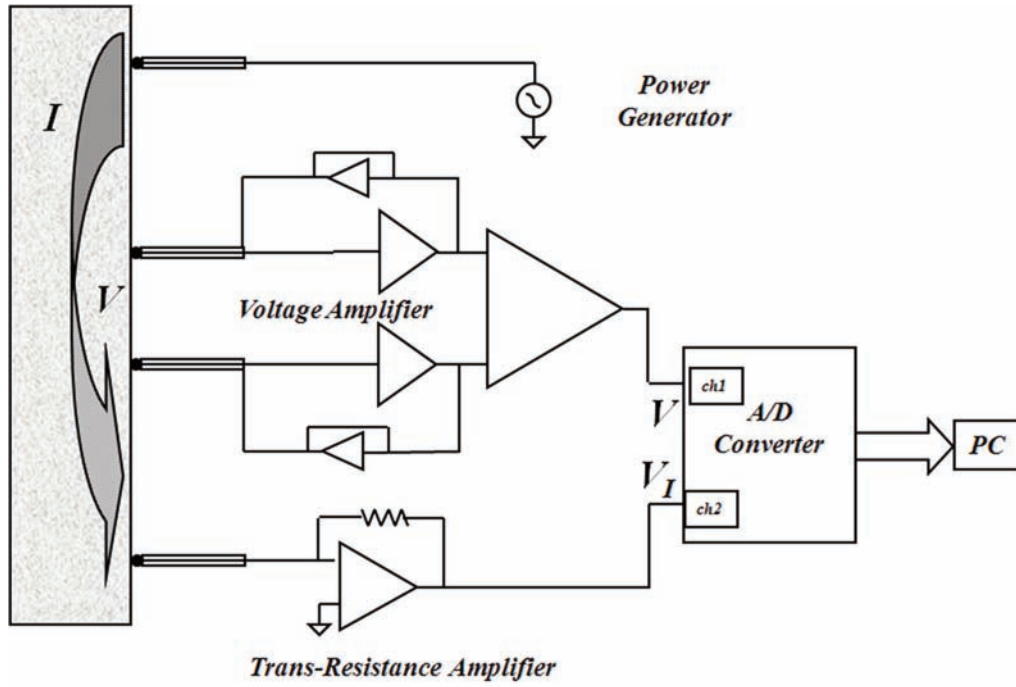


Figure 1. Block diagram of the measuring system that is composed of: a series of four electrodes laid on the material to be investigated; an analog circuit for the detection of signals, connected to a high voltage sinusoidal generator; a digital acquisition system; and a personal computer. The four electrodes are laid on the block of material to be analyzed. Two electrodes are used to generate and measure the injected current (at a selected frequency), while the other two electrodes are used to measure the potential difference. In this way, two voltages are obtained: the first proportional to the current; the second proportional to the difference of potential. These voltages are digitized through an analog–digital converter (A/D converter) connected to a personal computer (PC) for further processing. The real magnitudes hereby measured in the time domain are subsequently transformed into complex magnitudes in the frequency domain. From the ratio of the complex values, at the specific investigated frequency, it is possible to obtain the complex impedance. A program with an algorithm of numerical inversion allows the electrical resistivity and dielectric permittivity of the material to be obtained by measuring the transfer impedance; in this way, the reliability of the measured data is immediately analyzed, which is very useful during a measurement program.

the field. Quadripolar probes allow the measurement of electrical resistivity and dielectric permittivity using alternating current at LF ($30 \text{ kHz} < f < 300 \text{ kHz}$) or MF ($300 \text{ kHz} < f < 3 \text{ MHz}$). By increasing the distance between the electrodes, it is possible to investigate the electrical properties of sub-surface structures at greater depths. With the appropriate arrangements, measurements can be carried out with the electrodes slightly raised above the surface, providing completely nondestructive analysis, although also associated with greater errors. The probe can be used to perform immediate measurements on materials with high resistivity and permittivity, without the subsequent stages of data analysis.

In our recent study [Settimi et al. 2010], we proposed the theoretical modeling of the simultaneous and noninvasive measurement of electrical resistivity and dielectric permittivity using a quadrupole probe on a subjacent medium. A mathematical–physical model was applied on the propagation of errors in the measurement of resistivity and permittivity, based on the sensitivity functions tool. The findings were also compared with the results of the classical method of analysis in the frequency domain, which is useful for determining the behavior of zero and pole frequencies in the linear time-invariant circuit of the quadrupole. We underlined that the average values of electrical resistivity and dielectric permittivity can be used to estimate the complex

impedance over various terrains and concretes, especially when they are characterized by low levels of water saturation or content, and are analyzed within a frequency bandwidth ranging only from LF to MF. To meet the design specifications that are needed to ensure satisfactory performance of the probe, the forecasts of the sensitivity-functions approach are more reliable than the results foreseen by the transfer-functions method. In other words, once the measurement inaccuracy is bound by an acceptable limit (10%), the sensitivity approach provides more realistic values with respect to those provided by the transfer method. These numeric values concern both the band of frequency f for the probe and the measurable range of resistivity ρ or permittivity ϵ_r for the soils and concretes (the order of magnitude of these values is reported in the relevant literature; see Settimi et al. 2010, and references therein).

The present report (see also Earth-print.org and arXiv.org; Settimi et al. 2009) discusses the development and engineering of a suitable quadrupolar probe for simultaneous and noninvasive surveys of electrical resistivity and dielectric permittivity. The quadrupolar probe can perform measurements on a subsurface with inaccuracies below a fixed limit (10%) in a bandwidth of LF (100 kHz). The quadrupole should be connected to an appropriate ADC that can sample in phase and quadrature (IQ) [Jankovic and Öhman 2001] or in uniform mode. If the probe is

characterized by galvanic contact with the surface, the inaccuracies in the measurement of the resistivity and permittivity due to the IQ or uniform sampling ADC are analytically expressed. A large number of numerical simulations shows that the performances of the probe depends on the selected sampler, and that the IQ is better, compared to the uniform mode, under the same operating conditions, i.e. for bit resolution and medium.

This report is organized as follows. Following this introductory Section 1, Section 2 defines the data acquisition system. In Section 3, the theoretical modeling is provided for both the IQ (3.1) and the uniform (3.2) samplers. In Section 4, the design of the characteristic geometrical dimensions of the quadrupole probe is analyzed. Section 5 proposes a concluding discussion. Finally, the Appendix provides an outline of the somewhat lengthy calculations.

2. Data-acquisition system

To design a quadrupole probe (Figure 1) that can measure the electrical conductivity σ and the dielectric permittivity ϵ_r of a subjacent medium with inaccuracies below a prefixed limit (10%) in a band of low frequencies ($B = 100$ kHz), the probe needs to be connected to an appropriate ADC. Such an ADC should perform the IQ and uniform sampling [Razavi 1995, Jankovic and Öhman 2001] with bit resolution not exceeding 12, thereby rendering the system of measurement (voltage scale of 4 V) almost insensitive to the electrical noise of the external environment (≈ 1 mV).

The IQ can be implemented using a technique that is easier to achieve than for the uniform mode, because the voltage signal of the probe is in the frequency band of $B = 100$ kHz and the IQ is sampled with a rate of only $f_s = 4B = 400$ kHz, while, for example, low resolution uniform samplers are specified for rates of 5 MHz to 200 MHz.

With the aim of investigating the physics of the measuring system, the inaccuracies in the transfer impedance measured by the quadrupole probe due to uniform or IQ sampling ADCs are provided here.

For the stage downstream of the quadrupole, if the electrical voltage V is amplified, $V_v = A_v V$, and the intensity of the current I is transformed by a trans-resistance amplifier, $V_i = A_R I$, the signals having been processed by the sampler, then:

the inaccuracy $\Delta|Z|/|Z|$ for the modulus of the transfer impedance results from the negligible contributions of $\Delta A_v/A_v$ and $\Delta A_R/A_R$ for the voltage and trans-resistance amplifiers, respectively, and the predominant $\Delta|V_v|/|V_v|$ for the modulus of the voltage, due to the sampling,

$$\frac{\Delta|Z|}{|Z|} = \frac{\Delta A_v}{A_v} + \frac{\Delta A_R}{A_R} + 2 \frac{\Delta|V_v|}{|V_v|} \cong 2 \frac{\Delta|V_v|}{|V_v|}, \quad (2.1)$$

the inaccuracies for the modulus of the voltage and the current intensity being equal, $\Delta|V_v|/|V_v| = \Delta|V_i|/|V_i|$.

Instead, the inaccuracy $\Delta\Phi_z/\Phi_z$ for the initial phase of the transfer impedance coincides with the inaccuracy $\Delta\varphi_v/\varphi_v$ for the phase of the voltage, due to the sampler,

$$\frac{\Delta\Phi_z}{\Phi_z} = \frac{\Delta\varphi_v}{\varphi_v}, \quad (2.2)$$

the initial phase of the current being zero, $\varphi_i = 0$.

3. Theoretical modeling

Let us consider the IQ mode [Jankovic and Öhman 2001]. The IQ quartz is oscillating with a period T that is affected by an inaccuracy $\Delta T/T$. The quartz figure of merit $Q = T/\Delta T$ assumes high enough values, i.e. $1/Q \ll 1/(2\pi)$ [$Q = 10^4 - 10^6$]. It can be shown that the inaccuracy $\Delta|Z|/|Z|_{IQ}(n, \varphi_v)$ depends strongly on the bit resolution n , decreasing as the power function 2^{-n} of n , and weakly on the initial phase of voltage φ_v , such that (see also comments below Equation 3.7):

$$\begin{aligned} \frac{\Delta|Z|}{|Z|} \Big|_{IQ} &\cong \frac{1}{2^n} \left[1 + \frac{2\pi}{Q} \tan \varphi_v (1 + \cos 2\varphi_v) \right] = \\ &= \begin{cases} \frac{1}{2^n} \left(1 + \frac{2\pi}{Q} \right), & \varphi_v = \varphi_v^{\max} = \frac{\pi}{4} \\ \frac{1}{2^n} \left(1 - \frac{2\pi}{Q} \right), & \varphi_v = \varphi_v^{\min} = \pi - \varphi_v^{\max} \end{cases}, \end{aligned} \quad (3.1)$$

with $\Delta|Z|/|Z|_{IQ}(n, \varphi_v)$ being:

$$\lim_{\varphi_v \rightarrow \varphi_v^{\min}} \frac{\Delta|Z|}{|Z|} \Big|_{IQ} = \frac{1}{2^n} \quad (3.2)$$

in the limit value:

$$\varphi_v^{\min} = \arctg\left(\frac{Q}{4\pi}\right) \approx \frac{\pi}{2}. \quad (3.3)$$

Instead, for uniform sampling [Razavi 1995], the inaccuracy $\Delta|Z|/|Z|_U(n)$ for $|Z|$ only depends on the bit resolution n , decreasing as the power function 2^{-n} of n ,

$$\frac{\Delta|Z|}{|Z|} \Big|_U = \frac{1}{2^n}. \quad (3.4)$$

Consequently, for all ADCs with a bit resolution n :

if the probe performs measurements on a medium, then the inaccuracy $\Delta\epsilon_r/\epsilon_r(f)$ in the measurement of the dielectric permittivity ϵ_r is characterized by a minimum limit $\Delta\epsilon_r/\epsilon_r|_{\min}(\epsilon_r, n)$, which can be interpreted as the «physical bound» imposed on the inaccuracies of the problem, which depend on both ϵ_r and the bit resolution n , as it is directly proportional to the factor $(1 + 1/\epsilon_r)$, while it decreases as the power function 2^{-n} of n (Figure 2a);

if a probe with characteristic geometrical dimension L performs measurements on a medium with conductivity σ and permittivity ϵ_r , working within the cut-off frequency $f_T = f_T(\sigma, \epsilon_r) = \sigma/(2\pi\epsilon_0(\epsilon_r + 1))$ [Settimi et al. 2010], then the absolute error $E_{|Z|}(L, \sigma, n)$ in the measurement of the

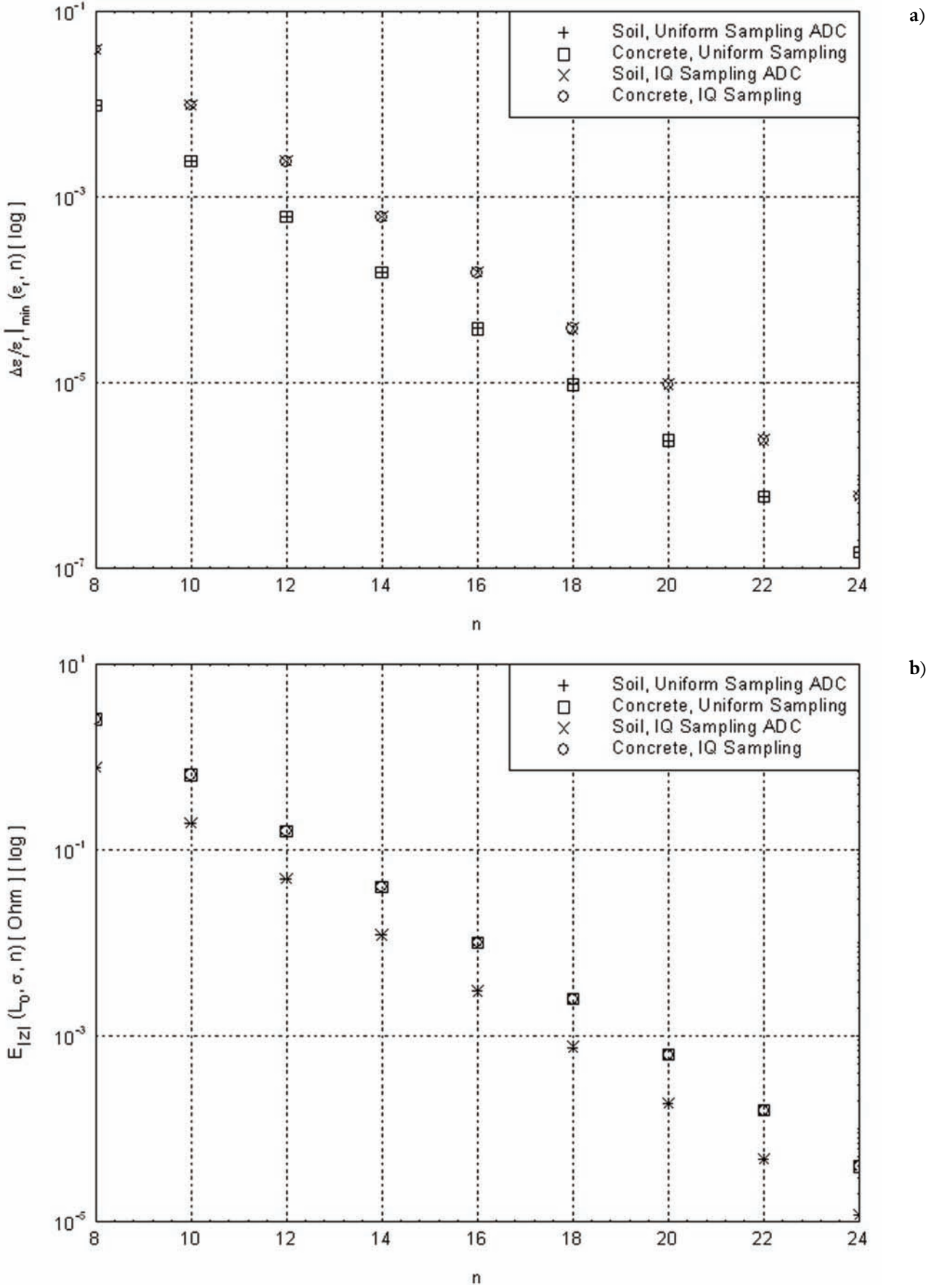


Figure 2. A quadrupole of characteristic geometrical dimension $L_0 = 1m$ has galvanic contact on a subsurface of dielectric permittivity around $\epsilon_r \approx 4$ and low electrical conductivity σ , like a nonsaturated terrestrial soil ($\sigma \approx 3.334 \cdot 10^{-4} S/m$) or concrete ($\sigma \approx 10^{-4} S/m$). With the hypothesis that the probe is connected to a sampler of bit resolution n , which ranges from 8 bit to 24 bit: (a) semi-logarithmic plot for the «physical bound» imposed on the inaccuracies, i.e. $\Delta \epsilon_r / \epsilon_r |_{\min}(\epsilon_r, n)$, as a function of the resolution n ; (b) semi-logarithmic plot for the absolute error $E_{|z|}(L_0, \sigma, n)$ for the transfer impedance in modulus below its cut-off frequency, as a function of the resolution n .

	U Sampling ADC	U Sampling			IQ Sampling
Soil	(12 bit, 10 MS/s)	(12 bit, 60 MS/s)	(12 bit, 200 MS/s)		(12 bit)
$(\epsilon_r = 4, \rho = 3000 \, \Omega \cdot m)$					
f_{opt}	150.361 kHz	267.569 kHz	387.772 kHz		≈ 1.459 MHz
f_{min}	92.198 kHz	98.042 kHz	95.055 kHz		94.228 kHz
f_{max}	265.287 kHz	885.632 kHz	≈ 1.832 MHz		≈ 16.224 MHz
Concrete	(8 bit, 50 MS/s)	(8 bit, 100 MS/s)	(8 bit, 250 MS/s)	(8 bit, 2 GS/s)	
$(\epsilon_r = 4, \rho = 10000 \, \Omega \cdot m)$					
f_{opt}	241.41 kHz	289.103 kHz	364.485 kHz	607.522 kHz	
f_{min}	98.574 kHz	96.629 kHz	95.553 kHz	94.953 kHz	
f_{max}	591.657 kHz	815.1 kHz	≈ 1.079 MHz	≈ 1.443 MHz	
Concrete	(12 bit, 5 MS/s)	(12 bit, 10 MS/s)	(12 bit, 60 MS/s)	(12 bit, 200 MS/s)	(12 bit)
$(\epsilon_r = 4, \rho = 10000 \, \Omega \cdot m)$					
f_{opt}	53.271 kHz	66.605 kHz	116.332 kHz	165.329 kHz	437.716 kHz
f_{min}	35.085 kHz	30.646 kHz	28.517 kHz	28.273 kHz	28.268 kHz
f_{max}	85.396 kHz	169.271 kHz	549.595 kHz	≈ 1.016 MHz	≈ 4.867 MHz

Table 1. With reference to the caption of Figure 3: a quadrupolar probe is connected to a uniform or IQ ADC (bit resolution n). Data are shown for the optimal working frequency, f_{opt} , that minimizes the inaccuracy in the measurement of permittivity, $\Delta\epsilon_r/\epsilon_r(f)$, minimum and maximum frequencies, f_{min} and f_{max} , that limit the inaccuracies of permittivity and conductivity, $\Delta\epsilon_r/\epsilon_r(f) \leq 0.1$ and $\Delta\sigma/\sigma(f) \leq 0.1$, for measurements performed on soil, with $n = 12$, and on concrete, with $n = 8$ and $n = 12$.

modulus for the transfer impedance $|Z|_N(L, \sigma)$ depends on σ , L and the bit resolution n , with the error inversely proportional to both σ and L , while it decreases as the power function 2^{-n} of n (Figure 2b).

Consider an IQ mode [Jankovic and Öhman 2001]. It can be shown that the inaccuracy $\Delta\Phi_Z/\Phi_Z|_{IQ}(n, \varphi_v)$ depends both on the bit resolution n , decreasing as the power function 2^{-n} of n , and on the voltage phase φ_v , such that (see also comments below Equation 3.7):

$$\begin{aligned} \frac{\Delta\Phi_Z}{\Phi_Z} \Big|_{IQ} &\cong \frac{1}{2^n} \frac{\sin(2\varphi_v)}{2\varphi_v} \left(1 + \frac{2\pi}{Q} \tan \varphi_v \right) = \\ &= \begin{cases} \frac{1}{2^n}, & \varphi_v = \varphi_v^{\max} = 0 \\ 0, & \varphi_v = \varphi_v^{\min} = \pi \end{cases}, \end{aligned} \quad (3.5)$$

with $\Delta\Phi_Z/\Phi_Z|_{IQ}(n, \varphi_v)$ being very low in $\varphi_v = \pi/2$, due to the high Q ,

$$\lim_{\varphi_v \rightarrow \pi/2} \frac{\Delta\Phi_Z}{\Phi_Z} \Big|_{IQ} = \frac{1}{2^{n-2}} \frac{1}{Q}. \quad (3.6)$$

Instead, for uniform sampling, the inaccuracy $\Delta\Phi_Z/\Phi_Z|_U(f, f_s)$ for Φ_Z depends on both the working frequency f of the probe and the rate sampling f_s of the ADC, with the inaccuracy directly proportional to the frequency ratio f/f_s ,

$$\frac{\Delta\Phi_Z}{\Phi_Z} \Big|_U = 2 \frac{f}{f_s}. \quad (3.7)$$

As a consequence, and only for uniform sampling ADCs, the inaccuracy $\Delta\Phi_Z/\Phi_Z(f, f_s)$ for the phase Φ_Z must be optimized in the upper frequency f_{up} , so when the probe performs measurements at the limit of its band $B, f_{up} = B$.

Let us provide some clues with respect the derivation of Equations (3.1) and (3.5). Ideally, a sinusoidal signal $V(t) = V_0 \cdot \sin(\omega t + \varphi_v)$ with an angular frequency $\omega = 2\pi/T$ and a period T can be sampled by an IQ mode. The in-phase $V_I = V(t=0) = V_0 \cdot \sin(\varphi_v)$ and quadrature $V_Q = V(t=T/4) = V_0 \cdot \cos(\varphi_v)$ values are obtained. The amplitude V_0 and phase φ_v of the sinusoidal signal are linked to the IQ values. Indeed: $V_0 = [(V_I)^2 + (V_Q)^2]^{1/2}$ and $\varphi = \arctg(V_I/V_Q)$. The inaccuracies of the IQ values $\Delta V_I/V_I = \Delta V_Q/V_Q = 1/2^{n+1}$ is defined by the bit resolution n of the IQ sampling. Applying the theory of error propagation, the inaccuracies of the amplitude V_0 and phase φ_v are derived. Indeed: $\Delta V_0/V_0 = 1/2^n$ and $\Delta\varphi_v/\varphi_v = 1/2^n \cdot [\sin(\varphi_v)/\varphi_v]$. More realistically, the quartz internal to the IQ sampler is oscillating with a period T that is affected by an inaccuracy $\Delta T/T$. Suppose that the merit figure of quartz $Q = T/\Delta T$ assumes high enough values, i.e. $1/Q \ll 1/(2\pi)$. The Taylor's series expansion to first order in $1/Q$ better approximates the values actually sampled, and in particular, the quadrature value $V_{Q,\Delta T} = V(t=T/4 + \Delta T)$, and consequently the amplitude $V_{Q,\Delta T} = [(V_I)^2 + (V_{Q,\Delta T})^2]^{1/2}$ and phase $\varphi_{\Delta T} = \arctg(V_I/V_{Q,\Delta T})$ of the sinusoidal signal. Indeed: $V_{Q,\Delta T} \approx V_Q - V_I \cdot (2\pi/Q)$, $V_{0,\Delta T} \approx V_0 \cdot [1 - (\pi/Q) \cdot \sin(2\varphi_v)]$ and $\tg\varphi_{\Delta T} \approx \tg\varphi_v \cdot [1 + (2\pi/Q) \cdot \tg(\varphi_v)]$. Moreover, the inaccuracy $\Delta T/T$ relative to the quartz merit figure $Q = 1/(\Delta T/T)$ increases the inaccuracy of the quadrature value to $\Delta V_{Q,\Delta T}/V_{Q,\Delta T} \approx \Delta V_Q/V_Q \cdot [1 + (4\pi/Q) \cdot \tg(\varphi_v)]$. Finally, in applying again the theory of error propagation, the inaccuracies of the amplitude $V_{0,\Delta T}$ and phase $\varphi_{V,\Delta T}$ are now derived in the case of a nonideal IQ quartz. So, some measurement inaccuracies similar to Equations (3.1) and (3.5) are derived: $\Delta V_{0,\Delta T}/V_{0,\Delta T} \approx \Delta V_0/V_0 \cdot [1 + (2\pi/Q) \cdot \tg(\varphi_v) \cdot (1 + 2\cos(2\varphi_v))]$ and $\Delta\varphi_{V,\Delta T}/\varphi_{V,\Delta T} \approx \Delta\varphi_v/\varphi_v \cdot [1 + (2\pi/Q) \cdot \tg(\varphi_v)]$.

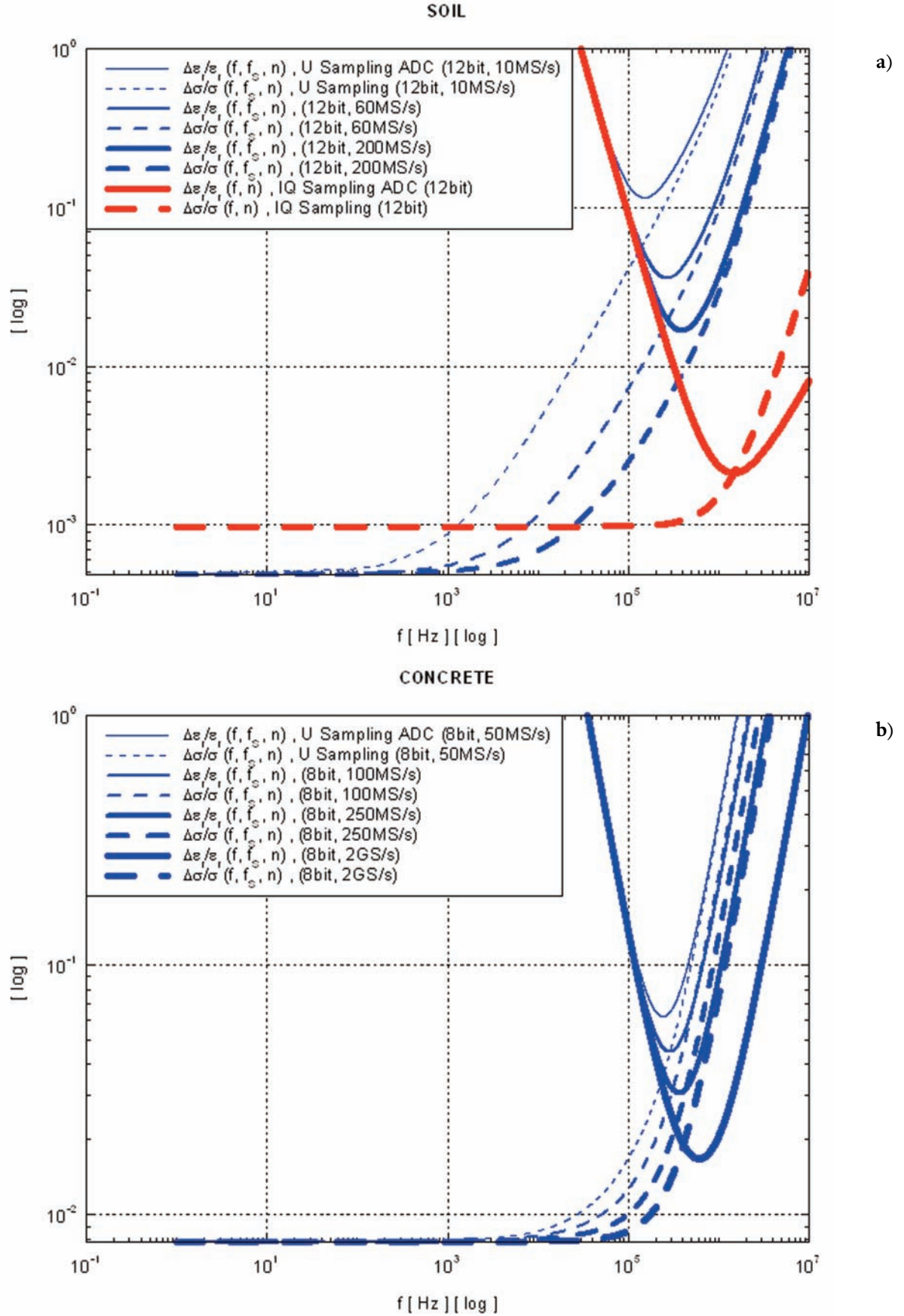
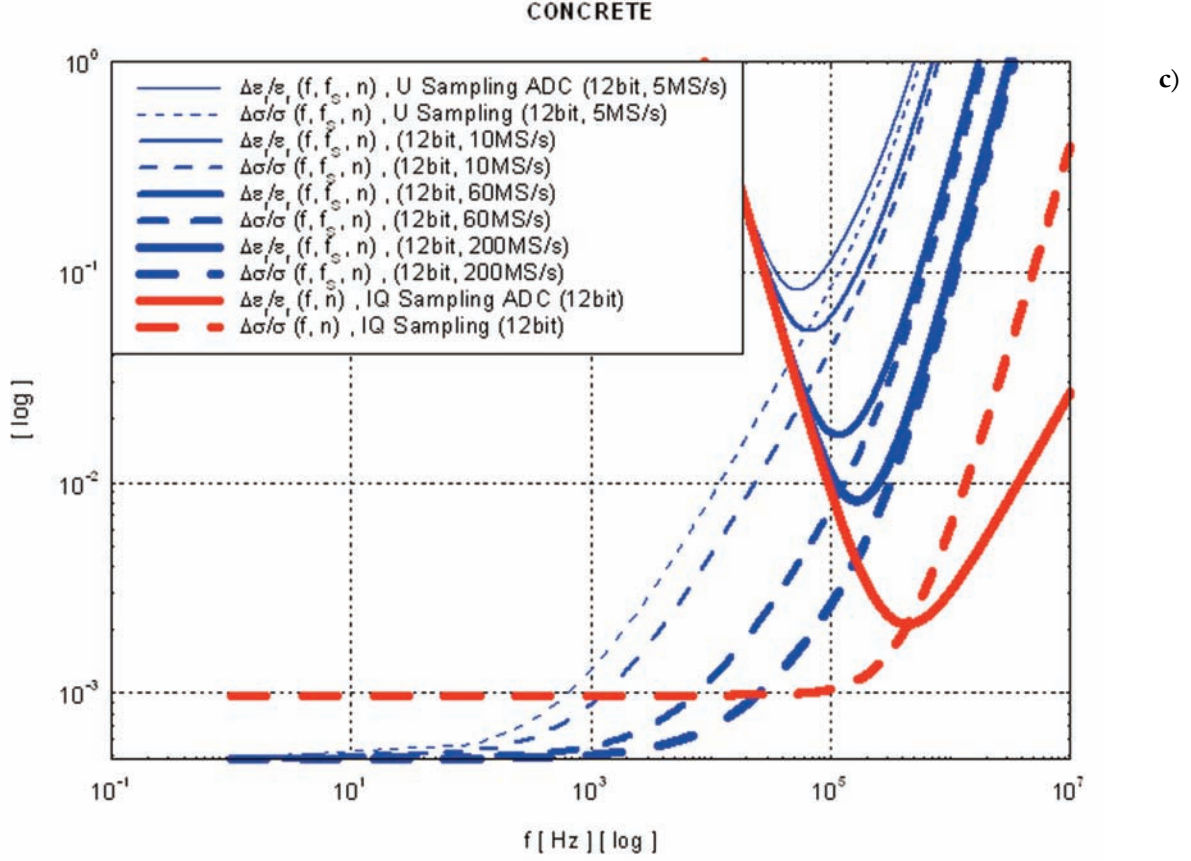


Figure 3 (this page and the next). With reference to the operating conditions described in the caption to Figure 2 (for quadrupole and subsurfaces). Bode's diagrams for the inaccuracies $\Delta\epsilon/\epsilon_r(f)$ and $\Delta\sigma/\sigma(f)$ in the measurements of the dielectric permittivity ϵ_r and the electrical conductivity σ , plotted as functions of the frequency f , for nonsaturated terrestrial soil (a) and concrete (b, c) analyses. The probe is connected to uniform or IQ or samplers (in the worst case, when the internal quartz is oscillating at its lowest merit factor $Q \approx 104$), of bit resolution $n = 12$ (a, c) or $n = 8$ (b), which allow inaccuracies in the measurements below a prefixed limit, of 15% (a, b) and 10% (a, c), within the frequency band $B = 100$ kHz (Table 1).



Continuing with the aim of investigating the physics of the measuring system, when the quadrupolar probe shows galvanic contact with the subjacent medium of electrical conductivity σ and dielectric permittivity ϵ_r , i.e. $h = 0$, and works in frequencies f lower than the cut-off frequency $f_T = f_T(\sigma, \epsilon_r)$ [Grard and Tabbagh 1991],

$$\Omega = \frac{\omega}{\omega_T} \leq 1, \quad (3.8)$$

the inaccuracies $\Delta\sigma/\sigma$ in the measurements of the conductivity σ and $\Delta\epsilon_r/\epsilon_r$ for the permittivity ϵ_r are analytically expressed (Figure 3; Table 1), and achievable connecting IQ or uniform samplers, which ensure the inaccuracies $\Delta|Z|/|Z|$ for the modulus $|Z|$, and $\Delta\Phi_Z/\Phi_Z$ for the phase Φ_Z of the transfer impedance [Settimi et al. 2010],

$$\frac{\Delta\sigma}{\sigma} \cong 2(1 + \Omega^2) \left(\frac{\Delta|Z|}{|Z|} + \frac{\Delta\Phi_Z}{\Phi_Z} \right), \quad (3.9)$$

$$\frac{\Delta\epsilon_r}{\epsilon_r} \cong 2(1 + \Omega^2) \left(1 + \frac{1}{\epsilon_r} \right) \left(\frac{1}{\Omega^2} \frac{\Delta|Z|}{|Z|} + \frac{\Delta\Phi_Z}{\Phi_Z} \right), \quad (3.10)$$

Only if the quadrupole probe is in galvanic contact with the subjacent medium, i.e. $h = 0$, then our mathematical-physical model predicts that the inaccuracies $\Delta\sigma/\sigma$ for σ and $\Delta\epsilon_r/\epsilon_r$ for ϵ_r are invariant in the linear (Wenner's) or square configuration, and independent of the characteristic geometrical dimension of the quadrupole, i.e. the electrode-electrode distance L [Settimi et al. 2010]. If besides grazing

the medium, the quadrupole measures σ and ϵ_r , working in a frequency f that is much lower than the cut-off frequency $f_T = f_T(\sigma, \epsilon_r)$, then the inaccuracy $\Delta\sigma/\sigma = F(\Delta|Z|/|Z|, \Delta\Phi_Z/\Phi_Z)$ is a linear combination of the inaccuracies $\Delta|Z|/|Z|$ and $\Delta\Phi_Z/\Phi_Z$ for the transfer impedance, while the inaccuracy $\Delta\epsilon_r/\epsilon_r = F(\Delta|Z|/|Z|)$ can be approximated as a linear function only of the inaccuracy $\Delta|Z|/|Z|$; in other words, if $f \ll f_T$, then $\Delta\Phi_Z/\Phi_Z$ is contributing in $\Delta\sigma/\sigma$ but not in $\Delta\epsilon_r/\epsilon_r$.

3.1. For IQ sampling

Let us consider IQ sampling ADCs (merit figure Q) [Jankovic and Öhman 2001]. The inaccuracy $\Delta\epsilon_r/\epsilon_r(f, n)$ in the measurement of permittivity ϵ_r is characterized by an optimal working frequency $f_{opt, IQ}(f_T)$, which is close to the cut-off frequency for the modulus of the transfer impedance $f_T = f_T(\sigma, \epsilon_r)$, i.e.

$$f_{opt, IQ} \cong f_T \left(1 + \frac{\pi/2}{Q} \right) \approx f_T. \quad (3.11)$$

This optimal frequency is tuned in a minimum value of inaccuracy $\Delta\epsilon_r/\epsilon_r|_{min, IQ}(\epsilon_r, n)$, which depends both on ϵ_r and on the specifications of the sampler, and in particular, its bit resolution n only. The minimum value of inaccuracy is directly proportional to the factor $(1 + 1/\epsilon_r)$, while decreasing as the power function $2^{-(n-3)}$ of n , such that (Figure 2a):

$$\frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{min, IQ} \cong \left(1 + \frac{1}{\epsilon_r} \right) \frac{1}{2^{n-3}} \left(1 + \frac{\pi}{Q} \right). \quad (3.12)$$

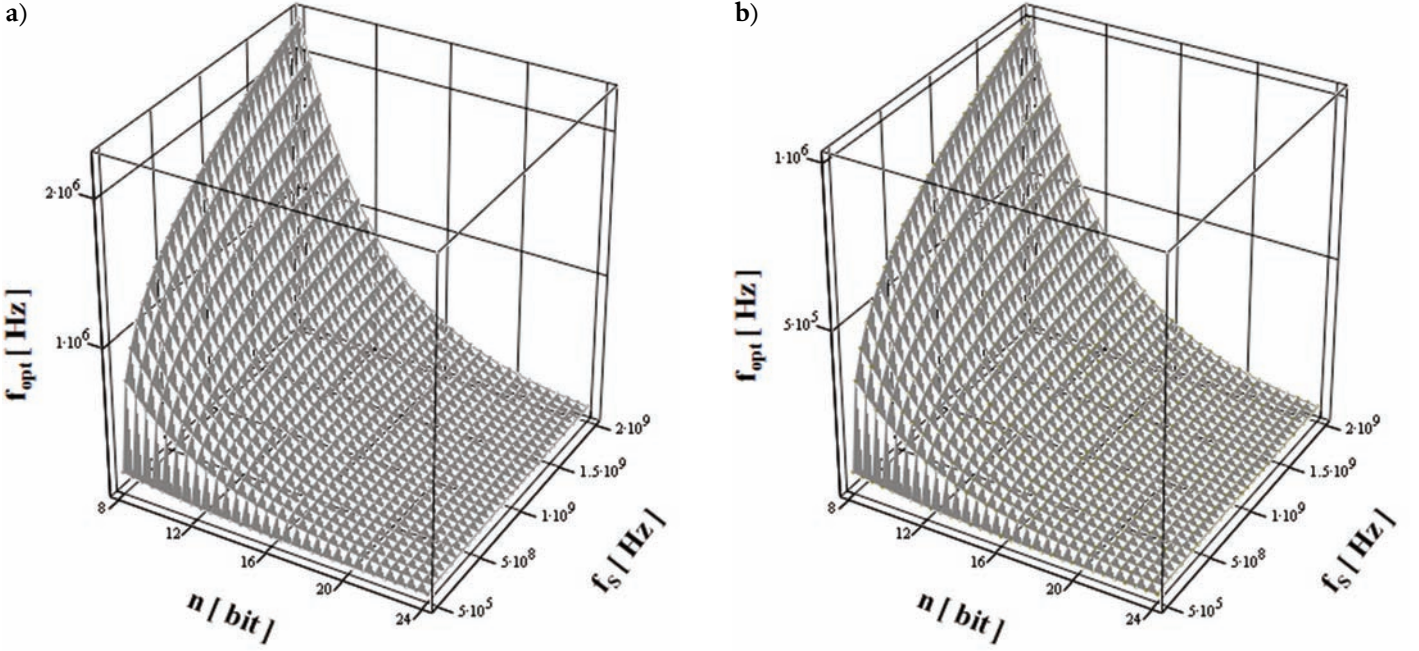


Figure 4. With reference to the operating conditions described in the caption to Figure 2 (for quadrupolar probe). Plots for the optimal working frequency $f_{opt,U}(n, f_s)$, which minimizes the inaccuracies in the measurements of dielectric permittivity, as functions of both the bit resolution n and the sampling rate f_s , for terrestrial soil (a) and concrete (b) analyses.

Consequently, if the frequency f of the probe is much lower than the cut-off frequency $f_T(\sigma, \epsilon_r)$ for the transfer impedance, then the inaccuracy $\Delta\sigma/\sigma(n)$ for σ is a constant, and the inaccuracy $\Delta\epsilon_r/\epsilon_r(f, n)$ for ϵ_r shows a downward trend in frequency, as $(f_T/f)^2$. Both these inaccuracies decrease as power functions of n , the first inaccuracy as $1/2^{n-2}$ and the second inaccuracy as $1/2^{n-1}$, i.e. (Figure 3; Table 1):

$$\frac{\Delta\sigma}{\sigma} \Big|_{IQ} \cong \frac{1}{2^{n-2}} \left(1 + \frac{\pi}{Q}\right), \quad \text{for } f \ll f_T, \quad (3.13)$$

$$\frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{IQ} \cong \left(1 + \frac{1}{\epsilon_r}\right) \frac{1}{2^{n-1}} \left(1 + \frac{2\pi}{Q}\right) \left[\frac{f_T}{f}\right]^2, \quad \text{for } f \ll f_T. \quad (3.14)$$

Even if the frequency f is much higher than $f_T(\sigma, \epsilon_r)$, it can be shown that the inaccuracies $\Delta\sigma/\sigma(f, n)$ and $\Delta\epsilon_r/\epsilon_r(f, n)$ do not deviate too much from an upward trend in frequency, as the parabolic curve $(f/f_T)^2$ (see also comments below Equations 3.15 and 3.16). The parable gradient is high for the σ measurement and low for the ϵ_r measurement. Indeed, both of these inaccuracies still decrease as power functions of n . The first inaccuracy decreases as $1/2^{n-2}$ and the second inaccuracy as $1/2^{n-1}$ (Figure 3; Table 1), i.e.:

$$\frac{\Delta\sigma}{\sigma} \Big|_{IQ} \cong \frac{1}{2^{n-2}} \left(1 + \frac{\pi}{Q}\right) \left[\frac{f}{f_T}\right]^2, \quad \text{for } f \gg f_T, \quad (3.15)$$

$$\frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{IQ} \cong \left(1 + \frac{1}{\epsilon_r}\right) \frac{1}{2^{n-1}} \left[\frac{f}{f_T}\right]^2, \quad \text{for } f \gg f_T. \quad (3.16)$$

A Mathcad program was run for the processing of some realistic values of the conductivity σ and permittivity ϵ_r for terrestrial soils and concretes. Mathcad numerically simulated

the inaccuracies in the measurements of σ and ϵ_r . The first pair of processed inaccuracies ($\Delta\sigma/\sigma, \Delta\epsilon_r/\epsilon_r$) consisted of the exact "complex" expressions reported by Settini et al. [2010], which hold for both LF and MF. The second pair of processed inaccuracies consists of the "simplified" Equations (3.9) and (3.10). As a first approximation, Equations (3.9) and (3.10) hold exactly for LFs ($f < f_T$), but not for MFs ($f > f_T$). Indeed, the program has shown that the numerical curves of Settini et al. [2010] overlap with the analytical curves of Equations (3.9) and (3.10). This overlap is excellent for $f < f_T$ and remains fine even for $f > f_T$.

Only if f is lower than f_T can the measurements then be optimized for ϵ_r and σ . A requirement might be that the inaccuracy $\Delta\epsilon_r/\epsilon_r(n, f)$ for ϵ_r is below the prefixed limit $\Delta\epsilon_r/\epsilon_r|_{fixed}$ (10%) within the frequency band $B = 100$ kHz. A minimum bit resolution $n_{min, IQ}(f_T, \epsilon_r)$ should be chosen. This minimum bit resolution depends on both f_T and ϵ_r and increases as the logarithmic function \log_2 of both of the ratios f_T/B and $1/\epsilon_r$, i.e.:

$$n_{min, IQ} \approx 1 - \log_2 \frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{fixed} + 2\log_2 \frac{f_T}{B} + \log_2 \left(1 + \frac{1}{\epsilon_r}\right). \quad (3.17)$$

Referring to the IQ sampling ADCs, the inaccuracies $\Delta\sigma/\sigma$ in the measurement of the electrical conductivity σ and $\Delta\epsilon_r/\epsilon_r$ for the dielectric permittivity ϵ_r were estimated for the worst case. So, the inaccuracies $\Delta|Z|/|Z|_{IQ}(n, \varphi_v)$ in the measurement of the modulus and $\Delta\Phi_Z/\Phi_Z|_{IQ}(n, \varphi_v)$ for the phase of the transfer impedance assume the mean and the maximum values, respectively; i.e. $\Delta|Z|/|Z|_{IQ} = \Delta\Phi_Z/\Phi_Z|_{IQ} = 1/2^n$.

To conclude, for the IQ mode, the optimal and

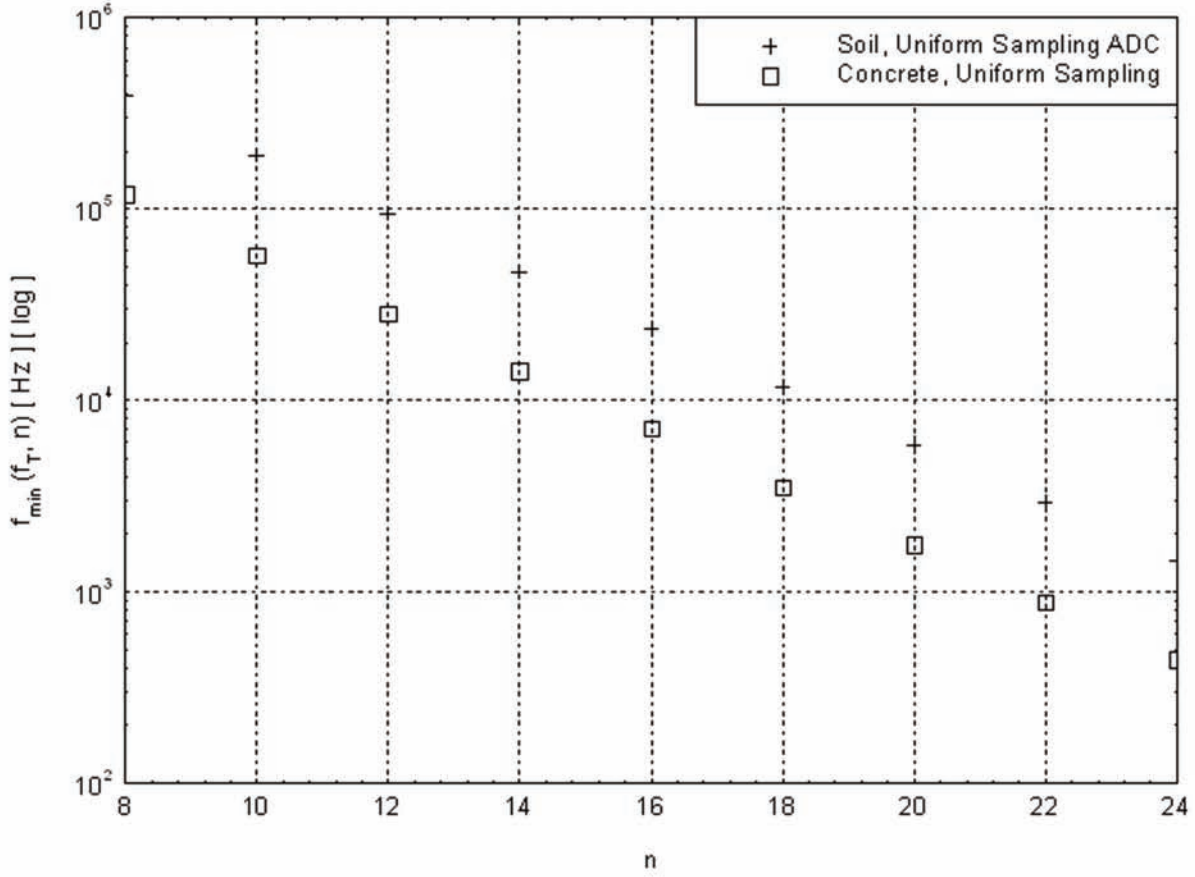


Figure 5. With reference to the operating conditions described in the caption to Figure 2 (for subsurface: nonsaturated terrestrial soil or concrete; sampling: uniform). Plot for the minimum values of frequency $f_{\min}(n, f_T)$ that allow inaccuracy in the measurement of the dielectric permittivity below a prefixed limit (10%), as a function of the bit resolution n [the cut-off frequency of the transfer impedance fixed as $f_T = f_T(\epsilon_r, \sigma)$, corresponding to the subsurface defined by the measurements (ϵ_r, σ)].

minimum values of the working frequency of the quadrupole probe interact in a competitive way. The more the quadrupole analyzes a subjacent medium characterized by a low electrical conductivity, with the aim of shifting the optimal frequency into a low band, the more the low conductivity has the self-defeating effect of shifting the minimum value of frequency into a higher band. Indeed, the probe can work around a low optimal frequency, which is achievable in measurements of transfer impedance with a low cut-off frequency, as is typical of materials characterized by low conductivity. Instead, the more the minimum value of the working frequency is shifted into a lower band, the more the minimum bit resolution for the sampler has to be increased. If the medium was selected, then increasing the inaccuracy for the measurement of the dielectric permittivity, or, if the inaccuracy was fixed, shifting the cut-off frequency into a higher band, i.e. selecting a medium with high conductivity. Finally, our analysis in the present report shows that the quadrupole can work at a low optimal frequency if the transfer impedance is characterized by a low cut-off frequency, which is in agreement with more traditional results in the literature [Grard 1990a, Grard 1990b, Grard and Tabbagh 1991, Tabbagh et al. 1993, Vannaroni et al. 2004, Del Vento and Vannaroni 2005]. However, the probe

can perform measurements in an appropriate band of higher frequencies centered around the cut-off frequency where the inaccuracy for the measurements of conductivity and permittivity were below a prefixed limit (10%).

3.2. For uniform sampling

Let us consider uniform sampling ADCs [Razavi 1995]. Suppose that the frequency f of the probe is lower than the cut-off frequency f_T for the modulus $|Z|(f, L)$ of the transfer impedance, i.e. $f_T = f_T(\sigma, \epsilon_r)$. It can be shown that the higher the bit resolution n , the more the optimal working frequency $f_{\text{opt}, U}(f_T, f_s, n)$ approximately depends on the cut-off frequency $f_T(\sigma, \epsilon_r)$. The optimal frequency $f_{\text{opt}, U}(f_T, f_s, n)$ minimizes the inaccuracy $\Delta\epsilon_r/\epsilon_r(f, f_s, n)$ in the measurement of the permittivity ϵ_r . Moreover, this optimal frequency depends on the specifications of the sampler, and in particular the sampling rate f_s and n . Finally, the frequency $f_{\text{opt}, U}(f_T, f_s, n)$ increases with both f_T and f_s , while decreasing as the power function $2^{-n/3}$ of n , such that (Figure 4):

$$\frac{f_{\text{opt}, U}}{f_T} \cong \sqrt[3]{\frac{1}{2^n} \frac{f_s}{f_T}}. \quad (3.18)$$

Moreover, the higher the bit resolution n , the more the inaccuracy $\Delta\epsilon_r/\epsilon_r(f, f_s, n)$ for ϵ_r cannot go down below a

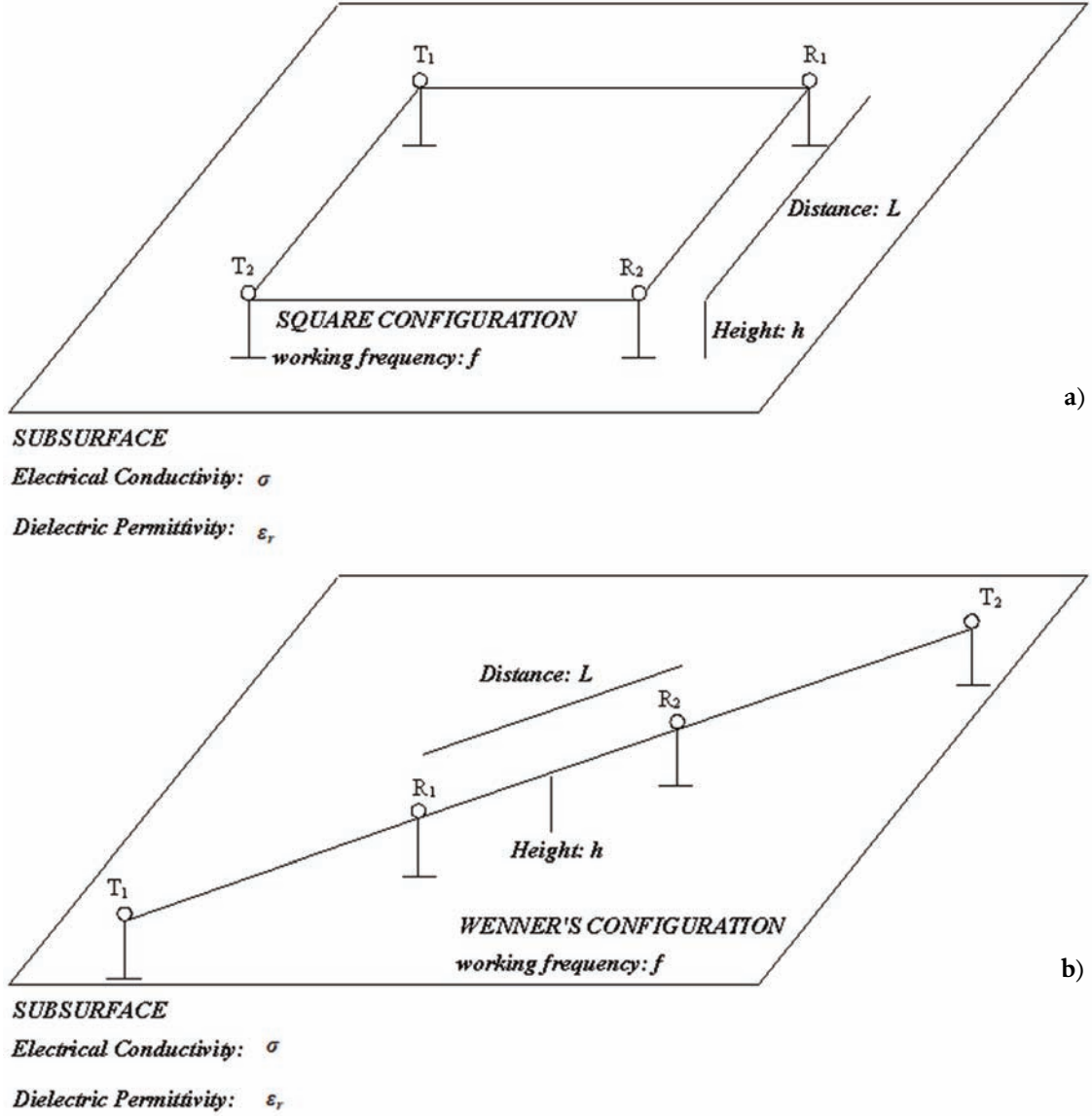


Figure 6. Quadrupolar probe in square (a) and linear (Wenner's) (b) configurations.

minimum limit of inaccuracy $\Delta\epsilon_r/\epsilon_r|_{\min,U}(\epsilon_r, n)$. This minimum limit of inaccuracy depends approximately on both ϵ_r and n , as it is directly proportional to the factor $(1+1/\epsilon_r)$, while decreasing as the power function $2^{-(n-1)}$ of n , similar to IQ sampling. The minimum value of inaccuracy $\Delta\epsilon_r/\epsilon_r|_{\min,U}(\epsilon_r, n)$ in the uniform mode is higher than the minimum inaccuracy $\Delta\epsilon_r/\epsilon_r|_{\min,IQ}(\epsilon_r, n)$ corresponding to the IQ mode (Figures 2a, 3; Table 1), i.e.:

$$\begin{aligned} \frac{\Delta\epsilon_r}{\epsilon_r} &\geq \frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{\min,U} \cong \left(1 + \frac{1}{\epsilon_r}\right) \frac{1}{2^{n-1}} \left[1 + \left(\frac{f_T}{f_{opt,U}}\right)^2\right] \gg \\ &\gg \frac{1}{4} \frac{\Delta\epsilon_r}{\epsilon_r} \Big|_{\min,IQ}, f_{opt,U} \ll f_T. \end{aligned} \quad (3.19)$$

Finally, the minimum value of frequency $f_{U,\min}(f_T, n)$ that allows an inaccuracy $\Delta\epsilon_r/\epsilon_r(f, f_S, n)$ below a prefixed limit $\Delta\epsilon_r/\epsilon_r|_{fixed}$ (10%) depends both on $f_T(\sigma, \epsilon_r)$ and n , as it is directly proportional to f_T , while it decreases as a power function of n , such that (Figure 5):

$$f_{\min,U} \cong \frac{f_T}{\sqrt{\frac{\Delta\epsilon_r/\epsilon_r|_{fixed}}{\Delta\epsilon_r/\epsilon_r|_{\min,U}} - 1}} < f_{opt,U}. \quad (3.20)$$

To conclude also on the uniform mode, the optimal frequency and the band of frequency of the quadrupolar probe interact in a competitive way. Indeed, an ADC with a high bit resolution is characterized by a low sampling rate, for which having selected the subjacent medium to be analyzed, the higher the resolution of the sampler used, with the aim of shifting the optimal frequency of the quadrupolar probe into a low band, the more the low sampling rate has the self-defeating effect of narrowing its frequency band. Moreover, a material with low electrical conductivity is usually characterized by low dielectric permittivity. Having designed the ADC, the more the quadrupole measures a transfer impedance limited by a low cut-off frequency, the more it can work at a low optimal frequency, even if centered

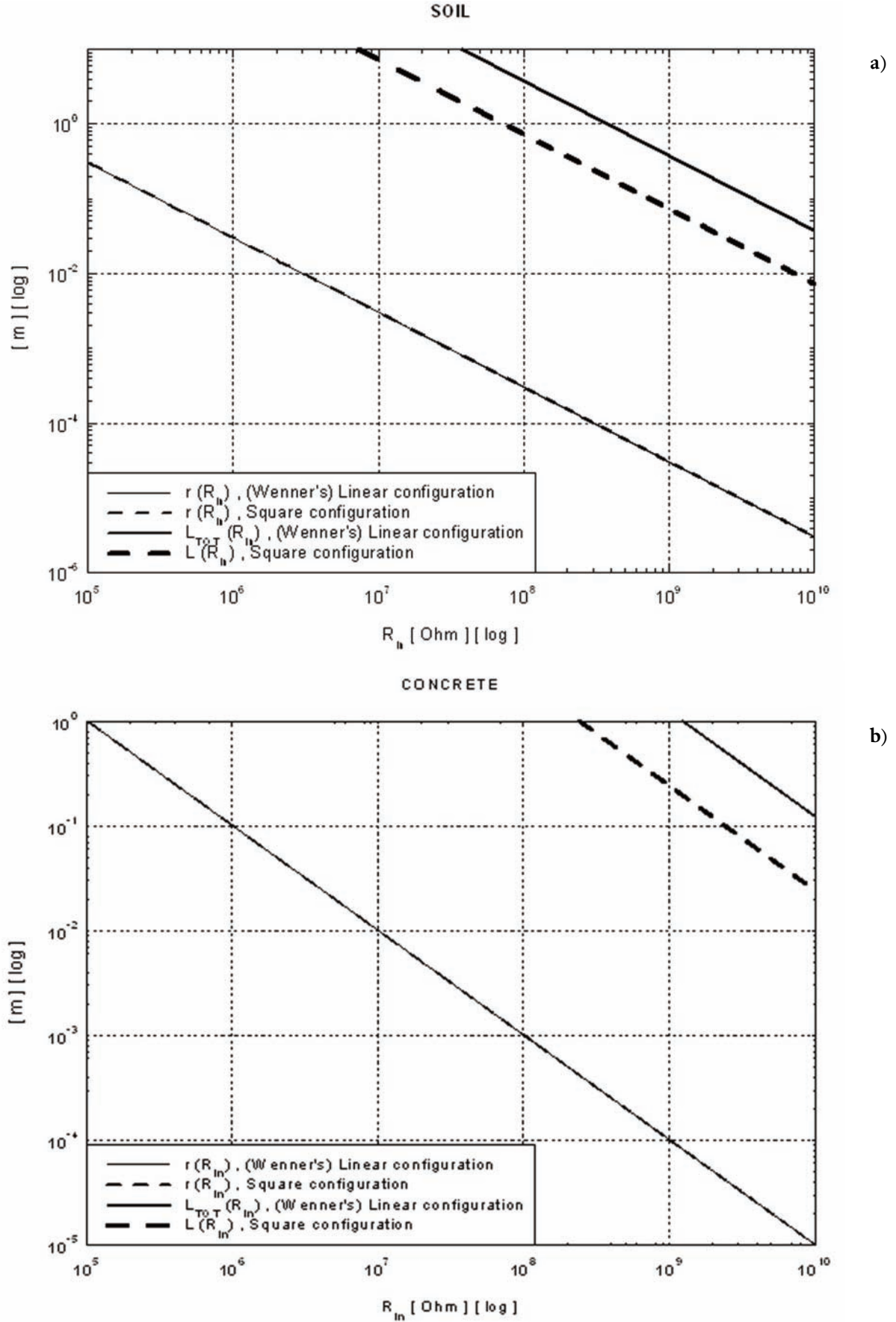


Figure 7. With reference to the operating conditions described in the caption to Figure 2 (for quadrupolar probe); the quadrupole is connected to an IQ sampler of minimum bit resolution $n_{min} = 12$ that allows inaccuracies in the measurements below a prefixed limit (10%) within the band $[f_{min}, B]$ from the minimum value of frequency f_{min} to $B = 100$ kHz. Like-Bode's diagrams of the radius $r(R_{in}, f_{min})$ for probe electrodes and of the characteristic geometrical dimension $L_s(r, n_{min})$ for square and of the length $L_{TOT}(r, n_{min}) = 3 \cdot L_W(r, n_{min})$ for (Wenner's) linear configurations, plotted as functions of the input resistance R_{in} for the amplifier stage, for nonsaturated terrestrial soil (a) and concrete (b); (Table 2).

	Square configuration	(Wenner's) Linear configuration
Soil		
$(\epsilon_r = 4, \rho = 3000 \Omega \cdot m)$		
$L, L_{TOT} = 3 \cdot L$	$L \approx 1 \text{ m}$	$L_{TOT} \approx 10 \text{ m}$
R_{in}	$72.8 \text{ M}\Omega$	$37.3 \text{ M}\Omega$
r	$417.042 \mu\text{m}$	$813.959 \mu\text{m}$
Concrete		
$(\epsilon_r = 4, \rho = 10000 \Omega \cdot m)$		
$L, L_{TOT} = 3 \cdot L$	$L \approx 1 \text{ m}$	$L_{TOT} \approx 1 \text{ m}$
R_{in}	$242 \text{ M}\Omega$	$1.24 \text{ G}\Omega$
r	$418.197 \mu\text{m}$	$81.616 \mu\text{m}$

Table 2. The radius r of the probe electrodes and characteristic geometrical dimension of the quadrupole for the square (side L) or Wenner's (length $L_{TOT} = 3L$) configurations, using an amplifier stage with input resistance R_{in} that is connected to an IQ sampling ADC with bit resolution $n = 12$, to perform measurements on soil or concrete.

on a narrow band. Finally, having selected the medium to be analyzed and having designed the sampler, the more the frequency band of the probe is widened, the more the inaccuracy of the measurements is increased.

4. Characteristic geometrical dimensions of the quadrupolar probe

In this section, we refer to Vannaroni et al. [2004], who discussed the dependence of the transmitting (TX) current and the reading (RX) voltage on the array and electrode dimensions. The dimensions of the quadrupolar probe terminals are not critical in the definition of the system, because they can be considered point electrodes with respect to their separating distances. In this respect, the separating distances to consider are either the square array side (Figure 6a) or the spacing distance for a Wenner configuration (Figure 6b). The only aspect that can be of importance for the practical implementation of the system is the relationship between the electrode dimensions and the magnitude of the current injected into the ground. The current is a critical parameter of the mutual impedance probe, in that in general, given the practical voltage levels applicable to the electrodes and the capacitive coupling with the soil, the current levels are expected to be quite low, with a resulting limit to the accuracy that can be achieved for the amplitude and phase measurements. Furthermore, low currents imply a reduction in the voltage signal read across the RX terminals and more stringent requirements for the reading amplifier.

The Appendix shows that once the input resistance R_{in} of the amplifier stage is fixed and the minimum value of frequency f_{min} for the quadrupole is selected (Figure 1), which allow an inaccuracy in the measurement of the dielectric permittivity ϵ_r below a prefixed limit (10%), then the radius

$r(R_{in}, f_{min})$ of the electrodes can be designed, as this depends only on the resistance R_{in} and the frequency f_{min} , as the radius is an inversely proportional function to both R_{in} and f_{min} (Figure 7; Table 2), as:

$$r \cong \frac{1}{(2\pi)^2 \epsilon_0 R_{in} f_{min}} . \quad (4.1)$$

Moreover, once the minimum bit resolution n_{min} for the IQ or uniform sampling ADC is known, which allows an inaccuracy for permittivity ϵ_r below the limit of 10%, then the electrode-electrode distance $L(r, n_{min})$ can also be defined, as this depends only on the radius $r(R_{in}, f_{min})$ and the bit resolution n_{min} , with the distance directly proportional to $r(R_{in}, f_{min})$ and increasing as the power function $2^{n_{min}}$ of n_{min} (Figure 7; Table 2),

$$L \propto r \cdot 2^{n_{min}} . \quad (4.2)$$

Finally, the radius $r(R_{in}, f_{min})$ remains invariant whether the probe assumes a linear (Wenner) or a square configuration. Once the resolution n_{min} is also given, then the distance $L_S(r, n_{min})$ in the square configuration must be smaller by a factor $(2 - 2^{1/2})$ compared to the corresponding distance $L_W(r, n_{min})$ in the Wenner configuration [Settimi et al. 2010]:

$$L_S = (2 - \sqrt{2}) \cdot L_W = (2 - \sqrt{2}) \cdot r \cdot 2^{n_{min}} . \quad (4.3)$$

5. Concluding discussion

This report has discussed the development and engineering of a suitable quadrupolar probe for simultaneous and noninvasive surveys of electrical resistivity and dielectric permittivity. The quadrupolar probe can perform measurements on a subsurface with inaccuracies below a fixed limit (10%) in a LF bandwidth (100 kHz). The quadrupole should be connected to an appropriate ADC that can sample

in IQ or in uniform mode. If the probe is characterized by galvanic contact with the surface, the inaccuracies in the measurements of resistivity and permittivity due to the IQ or uniform sampling ADC have been expressed analytically. A large number of numerical simulations have shown that the performance of the probe depends on the selected sampler, and that the IQ is better compared to the uniform mode under the same operating conditions, i.e. for bit resolution and medium (Figure 3; Table 1).

For the IQ mode, this is specified by an inaccuracy $\Delta\Phi_Z/\Phi_Z(n_{IQ})$ for the phase of the transfer impedance, which depends only on the bit resolution n_{IQ} , assuming small values (e.g., $\Delta\Phi_Z/\Phi_Z|_{\max}(12) = 1/2^{12} \approx 2.4 \cdot 10^{-4}$) over the entire frequency band $B = 100$ kHz of the quadrupole. For the uniform mode, the corresponding inaccuracy $\Delta\Phi_Z/\Phi_Z(f, f_s)$ depends on the frequency f , and it is only small for frequencies much lower than the sampling rate f_s [i.e. $2f/f_s \leq \Delta\Phi_Z/\Phi_Z|_{\max}(12)$]. The principal advantages of the IQ mode are: first, the minimum value $f_{\min}(n)$ of the frequency, which allows an inaccuracy for permittivity ϵ_r below 10%, is slightly lower when the probe is connected to an IQ rather than a uniform ADC, if all other operating conditions are equal, i.e. the resolution and the surface; and secondly, the inaccuracy $\Delta\sigma/\sigma$ for conductivity σ calculated in $f_{\min}(n)$ is smaller using IQ than with uniform sampling, as $\Delta\sigma/\sigma|_{IQ} < \Delta\sigma/\sigma|_U$, by almost one order of magnitude under the same operating conditions, and in particular for the resolution. As a minor disadvantage, the optimal frequency f_{opt} , which minimizes the inaccuracy for ϵ_r , is generally higher using IQ than uniform sampling, as $f_{opt, IQ} > f_{opt, U}$ of almost one MF decade, at most, under the same operating conditions, and in particular for the surface (Figure 3).

Instead, the uniform mode is specified by two degrees of freedom, the resolution of bit n_U and the rate of sampling f_s , compared to the IQ mode, which is characterized by one degree of freedom, the bit resolution n_{IQ} . Consequently the quadrupolar probe can be connected to a uniform ADC with a sampling rate f_s sufficiently fast at a resolution (for example $n_U = 8$) lower than for the IQ (i.e. $n_{IQ} = 12$) that it reaches the same prefixed limit of inaccuracy (i.e. 10%) in the measurement of the dielectric permittivity ϵ_r , for various media, and especially for those media with low electrical conductivities σ (Table 1).

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*Corresponding author: Alessandro Settimi,
Istituto Nazionale di Geofisica e Vulcanologia, Sezione Roma 2,
Roma, Italy; e-mail: alessandro.settimi@ingv.it.

Appendix

A series of two spherical capacitors with radius r and spacing distance $L \gg r$ is characterized by the electrical capacitance:

$$C = \frac{2\pi\epsilon_0}{\frac{1}{r} - \frac{1}{L-r}} \cong 2\pi\epsilon_0 r, \text{ for } L \gg r, \quad (\text{A.1})$$

with ϵ_0 the dielectric constant in a vacuum.

A quadrupole probe with four spherical electrodes of radius r and separating distance $L \gg r$ is arranged in the Wenner configuration with total length $L_{tot} = 3L$, which is specified by the pairs of transmitting electrodes T_1 and T_2 at the ends of the quadrupole and the reading electrodes R_1 and R_2 in the middle of the probe. The quadrupole probe is characterized by a capacitance that is almost invariant for the pairs of electrodes $T_{1,2}$ and $R_{1,2}$,

$$C_{T_1, T_2} = \frac{2\pi\epsilon_0}{\frac{1}{r} - \frac{1}{3L-r}} \cong C_{R_1, R_2} = \frac{2\pi\epsilon_0}{\frac{1}{r} - \frac{1}{L-r}} \cong C = 2\pi\epsilon_0 r, \text{ for } L \gg r. \quad (\text{A.2})$$

As the charge Q of the electrodes are equal, the electrical voltage across the pair T_1 and T_2 approximates the voltage between R_1 and R_2 ,

$$\Delta V_{T_1, T_2} \cong \Delta V_{R_1, R_2} \cong \frac{Q}{C}. \quad (\text{A.3})$$

For the equivalent capacitance circuit that schematizes the transmission stage of the quadrupole (Figure 8a), if the effect of the capacitance C across the electrodes is predominant relative to the shunted capacitances C_{T1} and C_{T2} , describing the electrical coupling between the transmitting electrodes and the subjacent medium as,

$$C \ll C_{T1} = C_{T2}, \quad (\text{A.4})$$

then, working in the frequency f , the probe injects into the medium a minimum bound for the modulus of the current $|I|_{min}$,

$$|I|_{min} \cong \omega \cdot C \cdot \Delta V_{T_1, T_2} = 2\pi f \cdot 2\pi\epsilon_0 r \cdot \Delta V_{T_1, T_2} = (2\pi)^2 \epsilon_0 r f \Delta V_{T_1, T_2}, \quad (\text{A.5})$$

with $|I|_{min}$ increasing linearly with f .

For the equivalent capacitance circuit that represents the reception stage of the quadrupole probe (Figure 8b), the effect of the capacitance C across the electrodes is predominant even relative to the shunted capacitances C_{R1} and C_{R2} , describing the coupling between the reading electrodes and the subjacent medium as,

$$C \ll C_{R1} = C_{R2}, \quad (\text{A.6})$$

If the quadrupole of electrode-electrode distance L is

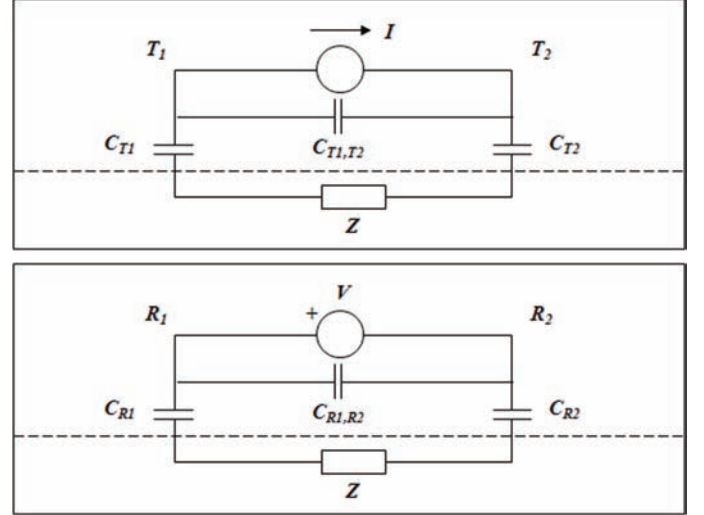


Figure 8. Equivalent capacitance circuits of the quadrupole probe that schematize the transmission (a) and reception (b) stages.

immersed in vacuum, then it can be characterized by the vacuum capacitance:

$$C_0 = 4\pi\epsilon_0 L, \quad (\text{A.7})$$

and, in the frequency f , measures a minimum limit $|Z|_{min}$ for the transfer impedance in modulus,

$$|Z|_{min} = \frac{1}{\omega \cdot C_0} = \frac{1}{2\pi f \cdot 4\pi\epsilon_0 L} = \frac{1}{2(2\pi)^2 \epsilon_0 L f}, \quad (\text{A.8})$$

which gives rises to a minimum for the electrical voltage $\Delta V_{min, R1, R2}$, flowing the current $|I|_{min}$,

$$\begin{aligned} \Delta V_{R1, R2}^{min} &= |Z|_{min} |I|_{min} \cong \\ &\cong \frac{1}{2(2\pi)^2 \epsilon_0 L f} \cdot (2\pi)^2 \epsilon_0 r f \Delta V_{T_1, T_2} = \frac{1}{2} \frac{r}{L} \Delta V_{T_1, T_2}. \end{aligned} \quad (\text{A.9})$$

Note that $\Delta V_{min, R1, R2}$ is independent of f , as $|I|_{min}$ is directly and $|Z|_{min}$ inversely proportional to f .

As a first finding, downstream of the probe the ADC must be specified by a bit resolution n , such that:

$$\frac{\Delta V_{R1, R2}^{min}}{\Delta V_{T_1, T_2}} \cong \frac{1}{2} \frac{r}{L} \approx \frac{\Delta V_{R1, R2}^{min}}{\Delta V_{R1, R2}} = \frac{1}{2^{n+1}} \Rightarrow \frac{r}{L} \approx \frac{1}{2^n}. \quad (\text{A.10})$$

Instead, if the quadrupole shows galvanic contact with a medium of electrical conductivity σ and dielectric permittivity ϵ_r working in a band lower than the cut-off frequency, i.e. $f_T = f_T(\sigma, \epsilon_r) = 1/2\pi \cdot \sigma / \epsilon_0(\epsilon_r + 1)$, then it measures the transfer impedance in the modulus

$$|Z| = \frac{1}{2\pi\sigma L}. \quad (\text{A.11})$$

As final findings, the voltage amplifier downstream of the probe must be specified by an input resistance R_{in} that is larger than both the transfer impedance, i.e.

$$R_{in} > |Z| = \frac{1}{2\pi\sigma L} \Rightarrow L > \frac{1}{2\pi\sigma R_{in}}, \quad (\text{A.12})$$

and the reactance associated with the capacitance C , which is characterized by a maximum value in the minimum of frequency f_{min} , i.e.

$$\begin{aligned} R_{in} &> \frac{1}{\omega_{min} C} = \frac{1}{2\pi f_{min} \cdot 2\pi \epsilon_0 r} = \\ &= \frac{1}{(2\pi)^2 \epsilon_0 r f_{min}} \Rightarrow r > \frac{1}{(2\pi)^2 \epsilon_0 R_{in} f_{min}}. \end{aligned} \quad (\text{A.13})$$